



Folded Metal Plate Monopole Antenna for Multiband Operation in the Mobile Phone

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ABSTRACT: A coupled feed printed monopole antenna with low profile yet covering the three LTE, four GSM, and UMTS band operation in the mobile phone is presented. Wideband operation with low profile is possible by exciting the monopole's wide radiating plate using coupled feed and short-circuiting it to the system ground plane of the mobile phone through a long meandered strip as an inductive shorting strip. The coupling feed contributes to a wide operating band to cover the frequency range of 1710 to 2690 MHz for the GSM 1800/1900/UMTS/LTE2300/LTE2500 operation. The inductive strip and dual band behaviour results in the generation of a wide operating band to cover the frequency range of 698 to 988 MHz for LTE-700, GSM-850, GSM-900. The planar monopole can be directly printed on the bottom no-ground portion of the system circuit board of the mobile phone and is promising to be integrated with a practical loudspeaker. The proposed antenna, including its planar and folded structures, are suitable for slim mobile phone applications.

Keywords: coupling feed, inductive shorting strip, printed monopole.

I. INTRODUCTION

Printed monopoles with a wide radiating strip are simple in design and have been shown to generate wideband operation for the multiband WWAN (wireless wide area network) communications for mobile phone applications. However, in order to cover the lower GSM bands, the radiating plate in the planar monopole usually occupies a large volume and is required to be in the folded structure to achieve a low profile for internal mobile phone antenna applications. In general, in addition to the large volume occupied, the thickness of the folded radiating plate is as large as 10 mm, which is not promising for applications in the modern slim mobile phone which generally requires its internal antenna to have a thin profile of 4 mm or less. When a planar radiating plate is used, it is reported that a planar monopole with a large size can have a wide operating band of 870–2450 MHz for the mobile phone. However, the large size will greatly limit its applications in the internal mobile phone antennas.

A novel planar monopole design having a small size yet capable of generating two wide operating bands to cover the eight-band LTE/GSM/UMTS operation in the mobile phone, which includes the LTE700 (698–787 MHz), GSM850 (824–894 MHz), GSM900 (880–960 MHz), GSM1800 (1710–1880 MHz), GSM1900 (1850–1990 MHz), UMTS (1920–2170 MHz), LTE2300 (2305–2400 MHz) and LTE2500 (2500–2690 MHz) bands is presented in this paper. Notice that the LTE (long term evolution) operation become attractive for the mobile users, as it can provide better mobile broad-band and multi-media services than the existing GSM and UMTS mobile networks. The proposed planar monopole can generate lower band with a large bandwidth to cover the frequency range of 698–960 MHz for the LTE-700, GSM-850, GSM-900 operation. The upper band can have an even larger bandwidth to cover the frequency range of 1710–2690 MHz for the GSM-1800/1900, UMTS, LTE-2300/2500 operation.

The proposed planar monopole is suitable to be directly printed on the bottom no-ground portion of the system circuit board of the mobile phone, making it easy to manufacture at low cost. The size of the wide radiating plate of the planar monopole is 12x40 mm² or 480 mm² only, which is much smaller than those in [1], [2] (both at least 1400 mm²). When including the 8-mm feed gap, the no-ground portion required in the proposed design is 20x40 mm² (800 mm²), which is

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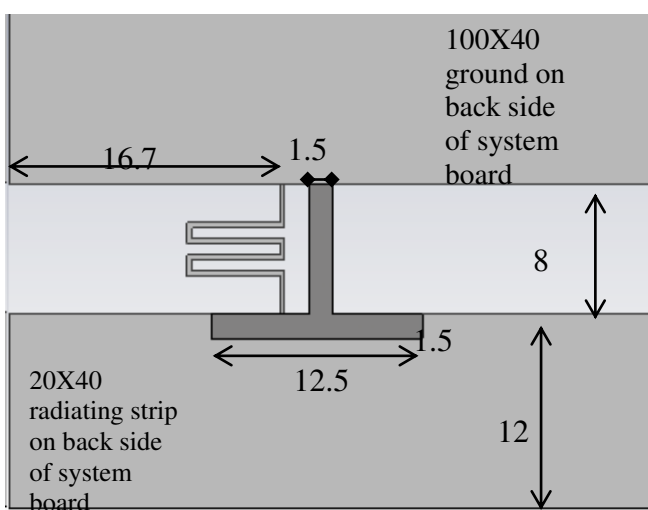
much less than that (1500 mm^2) in [9]. The antenna can also be integrated with nearby peripherals in a compact configuration. To achieve small size yet wideband operation, the proposed planar monopole is excited using a coupling feed and short-circuited to the system ground plane of the mobile phone through a long meandered strip as an inductive shorting strip. Detailed effects of the coupling feed and the inductive shorting strip are discussed in the communication.

Further, the radiating plate of the proposed antenna can be folded into a thin structure to occupy a small volume for the eight-band LTE/GSM/UMTS operation. In this case, by including the 8-mm feed gap between the radiating plate and the system ground plane of the mobile phone, the antenna also shows a low profile to the bottom edge of the ground plane. Details of the proposed antenna are presented.

II. PROPOSED ANTENNA

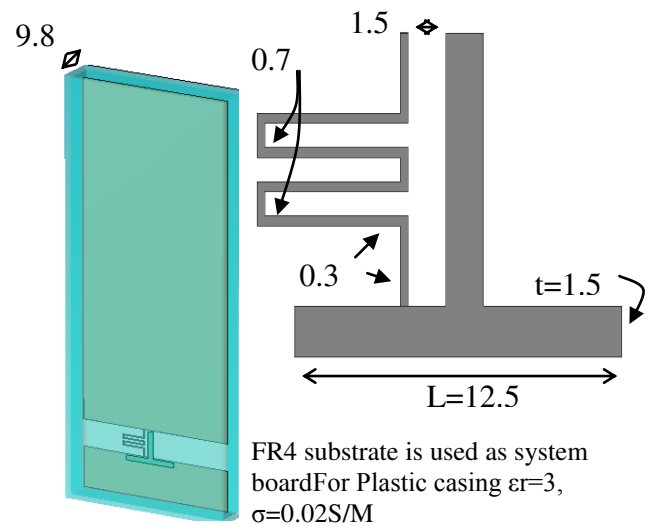
Fig. 1(a) shows the dimensional details of the proposed monopole with a coupling feed and an inductive shorting strip for the eight-band LTE/GSM/UMTS operation. Dimensions of the metal pattern of the antenna are given in Fig. 1(b). A 0.8-mm thick FR4 substrate with relative permittivity of 4.4 is used as the system circuit board of the mobile phone. The 1-mm thick plastic casing (relative permittivity 3.0 and conductivity 0.02 S/m) enclosing the circuit board as the plastic casing of a slim mobile phone has a thin profile of 9.8 mm. On the circuit board there is a printed system ground plane of size $40 \times 100 \text{ mm}^2$ and a no-ground portion of size $40 \times 20 \text{ mm}^2$. The planar monopole is printed on the bottom no-ground portion of the circuit board and comprises a wide radiating plate of size $12 \times 40 \text{ mm}^2$. Between the radiating plate and the ground plane, there is a feed gap of 8 mm. A simple coupling strip of length 12.5 mm, which is connected to the 50-ohm micro-strip feed line printed on the circuit board through a 8-mm long metal strip across the feed gap, capacitively excites the radiating plate. Across the feed gap, there is also a long meandered metal strip to short circuit the radiating plate to the ground plane. The meandered metal strip has a length of about 31 mm and a narrow width of 0.3 mm and behaves like a simple shorting strip loaded with a chip inductor. The meandered metal strip is hence considered as an inductive shorting strip here.

The coupling feed used in this design effectively compensates for the large inductive reactance over a wide frequency range, particularly over the desired upper band of 1710–2690 MHz. This leads to a very wide operating band obtained for the antenna's upper band to cover the GSM-1800, GSM-1900, UMTS, LTE-2300, and LTE-2500 operation. This coupling feed consequence is different from that applied for the internal WWAN antennas for mobile phone or notebook computer applications, in which the coupling feed mainly leads to enhanced bandwidth for the antenna's lower band at about 900 MHz or causes the excitation of the one-eighth-wavelength resonant mode as the antenna's lowest mode for the 900-MHz band operation.



(a)

Fig. 1.(a) Dimensional details of the proposed monopole



(b)

Fig. 1.(b) Plastic casing and coupling feed strip dimensions



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The coupling-feed effect obtained here is different because of the use of the wide radiating plate in the proposed design, which is different from the long, narrow radiating strips. A short (8mm) coupling T-strip protruded from the ground plane gives a different coupling-feed effect in the proposed design from the use of long coupling-feed strips.

By including the use of the inductive shorting strip, a wide lower band to cover the frequency range of 698–960 MHz for the LTE-700, GSM-850, and LTE-900 operation can be generated. Effects of the inductive shorting strip on the generation of the antenna's wide lower band are promising and should be selected properly to have desired bands. Also note that without the use of the wide radiating plate, that is, when the width of the radiating plate is decreased (the preferred width is 12 mm in this design), good impedance matching over the desired wide frequency range of 698–960 MHz cannot be achieved.

It is easy to fine-tune the desired lower and upper bands for the antenna to cover the eight-band LTE/GSM/UMTS operation, because even there are large effects of the inductive shorting strip on the antenna's lower band, the impedance matching for frequencies over the desired upper band of 1710–2690 MHz is relatively slightly affected. Moreover, the position of the monopole has an impact on generating the SAR. It is advantageous to place the antenna at the bottom edge of the system board as this gives the required less SAR values.

III. RESULTS

Fig. 2 shows the simulated return loss of the proposed antenna. The measured data agree with the simulated results obtained using CST MWS. With the -6dB S11 bandwidth definition, which is widely used as the design specification of the internal mobile phone antenna for WWAN communications, two wide operating bands are obtained.

The lower band shows a wide bandwidth of 480 MHz (690–1208 MHz), while the upper band has an even wider bandwidth of 1050 MHz (1670–2720 MHz). The wide lower and upper bands cover the LTE-700, GSM-850, GSM-900 and GSM-1800, GSM-1900, UMTS, LTE-2300 and LTE-2500 operation, respectively.

Fig. 3 shows the comparison of the simulated return loss for the proposed antenna, the case with an antenna at the top of the system board and the case with an antenna at the bottom of the system board. From the results of two positions, a much similar bandwidth for both is seen.

Fig. 4. Shows the simulated return loss as a function of length (L) of the coupling strip. It is obvious that as the length of the coupling strip increases, lower bandwidth is not enough to cover the desired frequency bands.

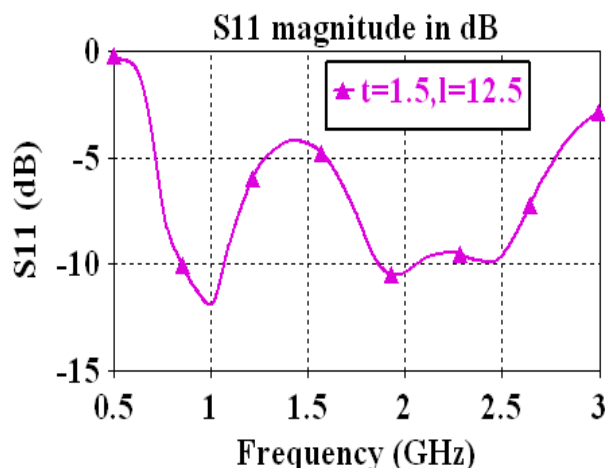


Fig. 2 simulated return loss of the proposed antenna.

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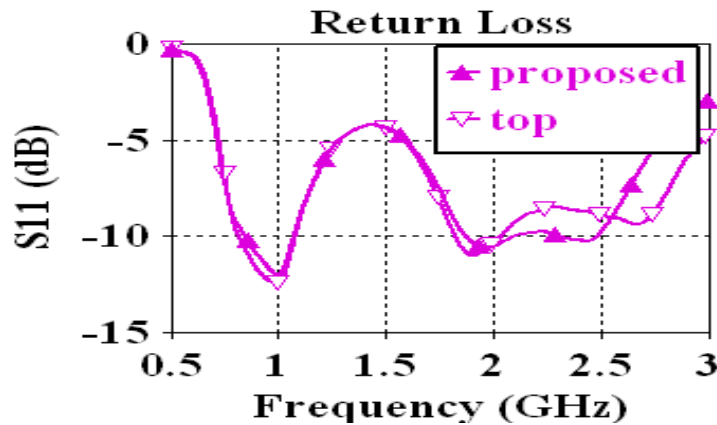


Fig.3 Simulated return loss as a function of the position of antenna on system board. Other dimensions are the same as in Fig. 1.

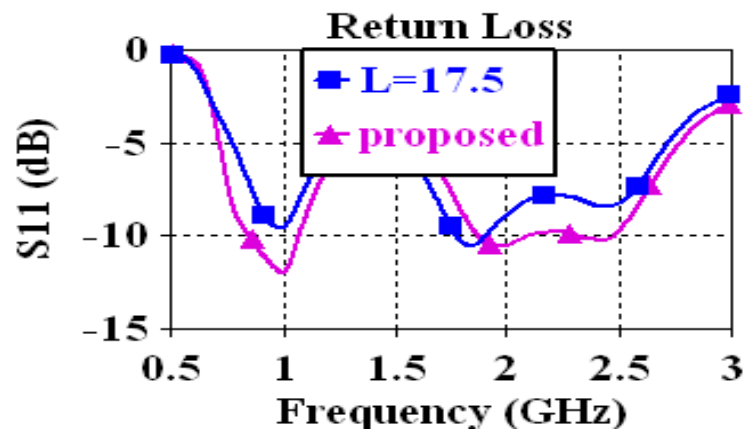


Fig.4 Simulated return loss as a function of the length L of the coupling strip. Other dimensions are the same as in Fig. 1

Fig 5. Shows the simulated return loss as a function of width (t) of the coupling strip. It is obvious that as the width of coupling strip increases, lower band decreases

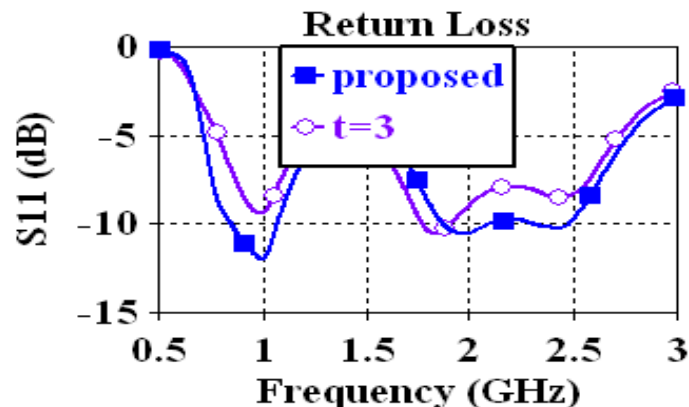


Fig.5 Simulated return loss as a function of the width t of the coupling strip.

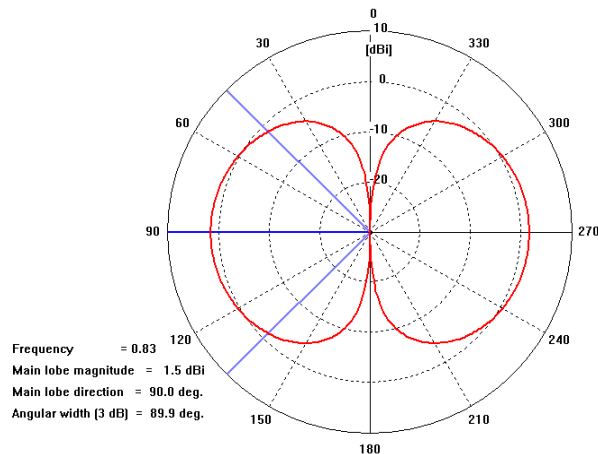


Fig.6 Simulated radiation characteristics of proposed antenna

IV. CONCLUSION

A planar monopole with a wide radiating strip energized by a coupling feed and short-circuited by an inductive metal strip has been shown to achieve low profile yet wideband operation for applications in the mobile phone to cover the eight-band LTE/GSM/UMTS operation. The proposed antenna can be in an all-printing structure or folded thin structure; both structures can provide two wide operating bands to cover the desired frequency ranges of 698–960 and 1710–2690 MHz. The obtained results indicate that the proposed antenna is suitable to be applied in the modern slim mobile phone for the eight-band LTE/GSM/UMTS operation.

REFERENCES

- [1] C. C. Lin, H. C. Tung, H. T. Chen, and K. L. Wong, "A folded metalplate monopole antenna for multi-band operation of a PDA phone," *Microw. Opt. Technol. Lett.*, vol. 39, pp. 135–138, Oct. 20, 2003.
- [2] S. Y. Lin, "Multiband folded planar monopole antenna for mobile handset," *IEEE Trans. Antennas Propag.*, vol. 52, pp. 1790–1794, Jul. 2004.
- [3] R. A. Bhatti and S. O. Park, "Octa-band internal monopole antenna for mobile phone applications," *Electron. Lett.*, vol. 44, pp. 1447–1448, Dec. 4, 2008.
- [4] R. A. Bhatti, Y. T. Im, J. H. Choi, T. D. Manh, and S. O. Park, "Ultrathin planar inverted-F antenna for multistandard handsets," *Microw. Opt. Technol. Lett.*, vol. 50, pp. 2894–2897, Nov. 2008.
- [5] J. Villanen, C. Icheln, and P. Vainikainen, "A coupling element-based quad-band antenna structure for mobile handsets," *Microw. Opt. Technol. Lett.*, vol. 49, pp. 1277–1282, Jun. 2007.
- [6] K. L. Wong, Y. C. Lin, and B. Chen, "Internal patch antenna with a thin air-layer substrate for GSM/DCS operation in a PDA phone," *IEEE Trans. Antennas Propag.*, vol. 55, pp. 1165–1172, Apr. 2007.
- [7] K. L. Wong, Y. C. Lin, and T. C. Tseng, "Thin internal GSM/DCS patch antenna for a portable mobile terminal," *IEEE Trans. Antennas Propag.*, vol. 54, pp. 238–242, Jan. 2006.
- [8] M. F. Abedin and M. Ali, "Modifying the ground plane and its effect on planar inverted-F antennas (PIFAs) for mobile phone handsets," *IEEE Antennas Wireless Propag. Lett.*, vol. 2, pp. 226–229, 2003.
- [9] Z. Du, K. Gong, and J. S. Fu, "A novel compact wide-band planar antenna for mobile handsets," *IEEE Trans. Antennas Propag.*, vol. 54, pp. 613–619, Feb. 2006.
- [10] S. Sesia, I. Toufik, and M. Baker, Eds., *LTE, The UMTS Long Term Evolution: From Theory to Practice*. New York: Wiley, 2009. [
- [11] K. L. Wong, *Planar Antennas for Wireless Communications*. New York: Wiley, 2003.
- [12] K. L. Wong and C. H. Huang, "Bandwidth-enhanced internal PIFA with a coupling feed for quad-band operation in the mobile phone," *Microw. Opt. Technol. Lett.*, vol. 50, pp. 683–687, Mar. 2008.
- [13] C. H. Chang and K. L. Wong, "Internal coupled-fed shorted monopole antenna for GSM850/900/1800/1900/UMTS operation in the laptop computer," *IEEE Trans. Antennas Propag.*, vol. 56, pp. 3600–3604, Dec. 2008.
- [14] K. L. Wong and C. H. Huang, "Printed PIFA with a coplanar coupling feed for penta-band operation in the mobile phone," *Microw. Opt. Technol. Lett.*, vol. 50, pp. 3181–3186, Dec. 2008.
- [15] K. L. Wong and S. J. Liao, "Uniplanar coupled-fed printed PIFA for WWAN operation in the laptop computer," *Microw. Opt. Technol. Lett.*, vol. 51, pp. 549–554, Feb. 2009.
- [16] C. T. Lee and K. L. Wong, "Uniplanar coupled-fed printed PIFA for WWAN/WLAN operation in the mobile phone," *Microw. Opt. Technol. Lett.*, vol. 51, pp. 1250–1257, May 2009.
- [17] K. L. Wong and C. H. Huang, "Compact multiband PIFA with a coupling feed for internal mobile phone antenna," *Microw. Opt. Technol. Lett.*, vol. 50, pp. 2487–2491, Oct. 2008.



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- [18] C. H. Chang and K. L. Wong, “Printed PIFA for penta-band WWAN operation in the mobile phone,” IEEE Trans. Antennas Propagat., vol. 57, pp. 1373–1381, May 2009.
- [19] C. H. Wu and K. L. Wong, “Internal hybrid loop/monopole slot antenna for quad-band operation in the mobile phone,” Microw. Opt. Technol. Lett., vol. 50, pp. 795–801, Mar. 2008.
- [20] Y. W. Chi and K. L. Wong, “Half-wavelength loop strip fed by a printed monopole for penta-band mobile phone antenna,” Microw. Opt. Technol. Lett., vol. 50, pp. 2549–2554, Oct. 2008.
- [21] M. R. Hsu and K. L. Wong, “WWAN ceramic chip antenna for mobile phone application,” Microw. Opt. Technol. Lett., vol. 51, pp. 103–110, Jan. 2009.
- [22] C. H. Wu and K. L. Wong, “Internal shorted planar monopole antenna embedded with a resonant spiral slot for penta-band mobile phone application,” Microw. Opt. Technol. Lett., vol. 50, pp. 529–536, Feb. 2008.